

## PETROPHYSICS VOLVE 15/9-F-10

### 1 Modell

Well 15/9-F-10 is evaluated accordingly to the Model reported in : Sleipner Øst and Volve Model 2006, Hugin and Skagerak Formation , Petrophysical Evaluation, Document 3781-06, 2006-11-10, Authors: E. Solfjell, K.A. Lehne

#### 1.1 Porosity

The porosity is derived from the density log which is calibrated to overburden corrected core porosity for wells drilled with OBM and WBM.. The neutron log has been used to correct for mud filtrate invasion. The equation in use is:

$$Phif = Phid + A*(Nphi-Phid) + B$$

Here A and B are regression constants. Phid is the density porosity.

$$Phid = (Rhoma - Rhob) / (Rhoma - Rhofl).$$

#### 1.2 Clay Volume

The Clay volume is entirely derived from the gamma ray log GR. The function used is the linear relationship :

$$VSH = (GRmax - GR) / (GRmax - GRmin) \quad (\text{API units})$$

Grmax : Gamma ray Claystone . Grmin : Gamma ray clean Sandstone.

### 1.3 Water Saturation

The water saturation is evaluated with the Archie formula :

$$S_w = (a \cdot R_w / R_t \cdot \text{Phif}^m)^{1/n}$$

Here  $S_w$  = Water saturation,  $a$  = Archies lithology konst.,  $R_w$  = Formation Water Resistivity,  
 $R_t$  = True Resistivity,  $\text{Phif}$  = porosity,  $m$  = cementation exponent,  $n$  = saturation exponent.

### 1.4 Permeability

Permeability is based on multivariable regression analysis between log porosity and shale volume against overburden corrected core permeability., The following functions are being used on the Volve Field :

$K_{logh} = 10^{(8 \cdot \text{Phif} - 9 \cdot V_{sh} + 2)}$	Hugin
$K_{logh} = 10^{(32 \cdot \text{Phif} - 2 \cdot V_{sh} - 3)}$	Sleipner *
$K_{logh} = 10^{(17.4 \cdot \text{Phif} - 3 \cdot V_{sh} - 1.85)}$	Skagerak*

\* Not in this well

### 1.5 Sand definition

For oil/water filled Hugin Fm :

$\text{Phif} < 0.10$  ,  $V_{sh} > 0.50$ . These corresponding to overburden corrected core permeability of 0.5 mD. - Local modifications by manual editing, might also have been done.

## 1.6 Evaluation parameters

The different evaluation parameter are seen in table 1.

Tab 1.

Evaluation Parameters 15/9-F10				
Parameter	Draupne	Heather	Hugin	Smith Bank
Rhoma	2.66	2.66	2.65	2.65
Rhofl	1	1	0.9	0.9
A	0	0	0.4	0.4
B	0	0	0.01	0.01
Grmin	20	20	20	20
Grmax	120	120	120	120
a	1	1	1	1
n	2	2	2.45	2.45
m	2	2	*	*
* $m = 1.865 * (Klogh^{**} - 0.0083)$				
Rw = 0.07 ohmm at 20 °C, Temp Gradient : 2.6 °C				
Reservoir Temperature : 111 °C at 2800m TVDSS.				

## 2 Results

### 2.1 Petrophysical Parameters from Log Evaluation 15/9-F-10

Petrophysical Parameters						
Formation	NetGros	Phif	Sw.	Klogh_A *	Klogh_H	Klogh-G
Hugin	0.997	0.24	0.997	5870	281	3394

\*A: Aritmetic , H: Harmonic , G: Geometric

## **2.2 CPI**

Volve 15/9-F-10  
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 STATOILHYDRO

